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Zeng

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(54) **LANE FUSION SYSTEM USING FORWARD-VIEW AND REAR-VIEW CAMERAS**

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B60W 40/06 (2012.01)
G06K 9/00 (2006.01)

(52) **U.S. Cl.**
CPC **B60W 40/06** (2013.01); **G06K 9/00798** (2013.01); **B60W 2550/146** (2013.01)

(58) **Field of Classification Search**
USPC 348/149
See application file for complete search history.

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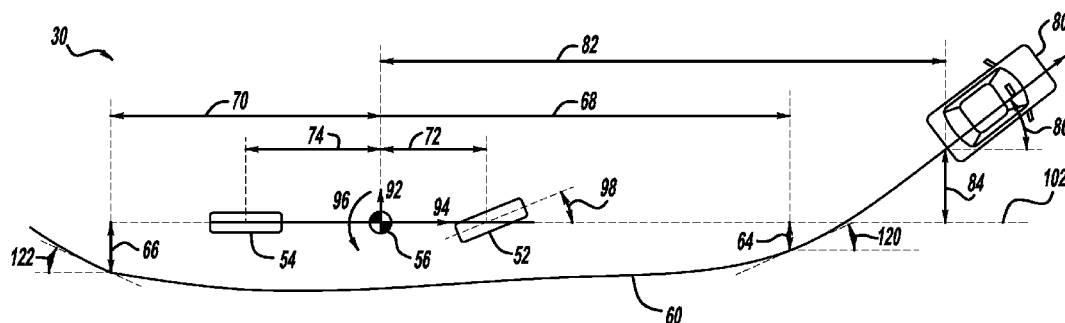|				
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(57) **ABSTRACT**

A method and system for computing lane curvature and a host vehicle's position and orientation relative to lane boundaries, using image data from forward-view and rear-view cameras and vehicle dynamics sensors as input. A host vehicle includes cameras at the front and rear, which can be used to detect lane boundaries such as curbs and lane stripes, among other purposes. The host vehicle also includes vehicle dynamics sensors including vehicle speed and yaw rate. A method is developed which computes lane curvature and the host vehicle's position relative to a lane reference path, where the lane reference path is derived from the lane boundaries extracted from a fusion of the front and rear camera images. Mathematical models provided in the disclosure include a Kalman filter tracking routine and a particle filter tracking routine.
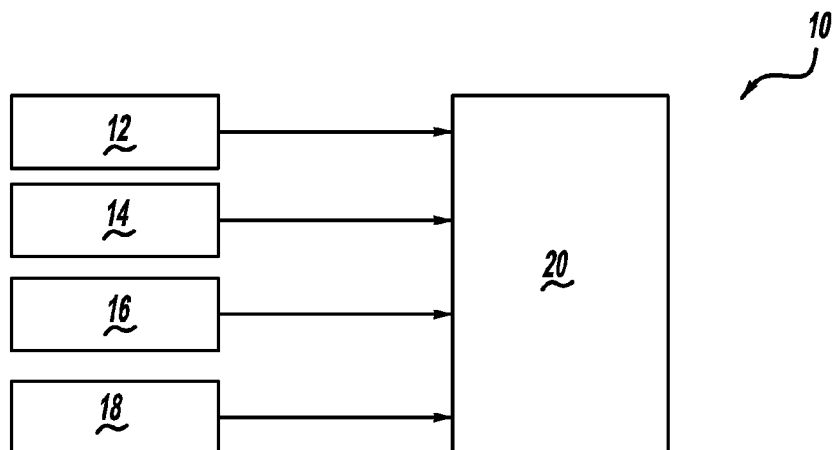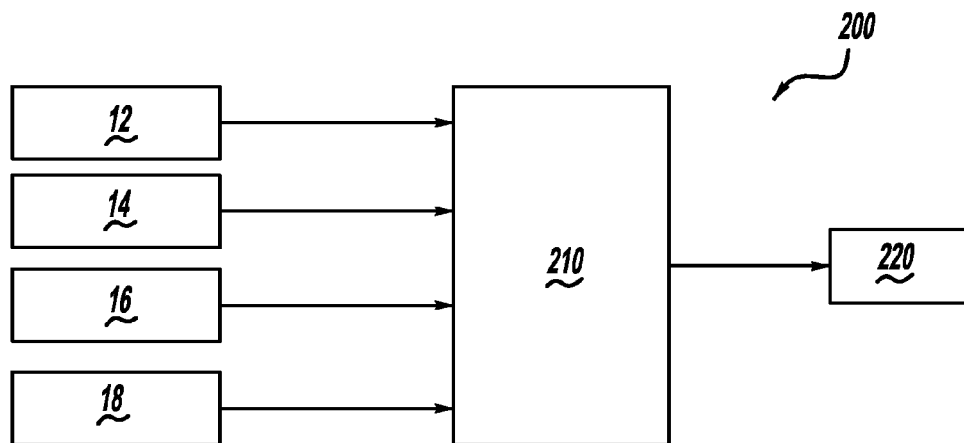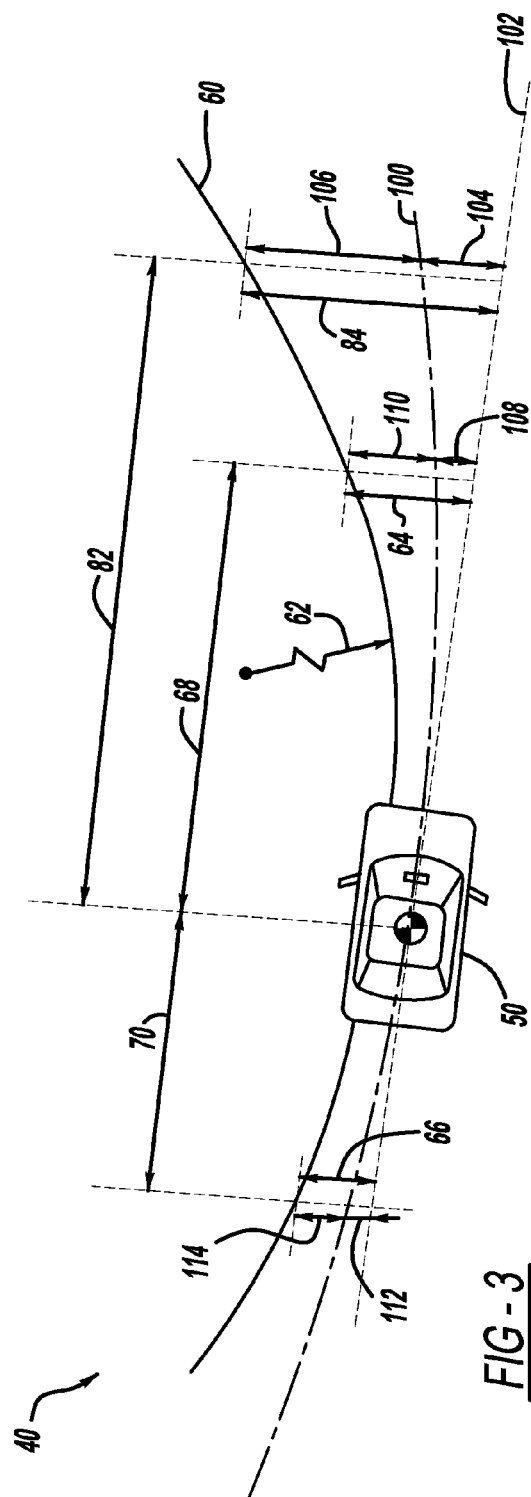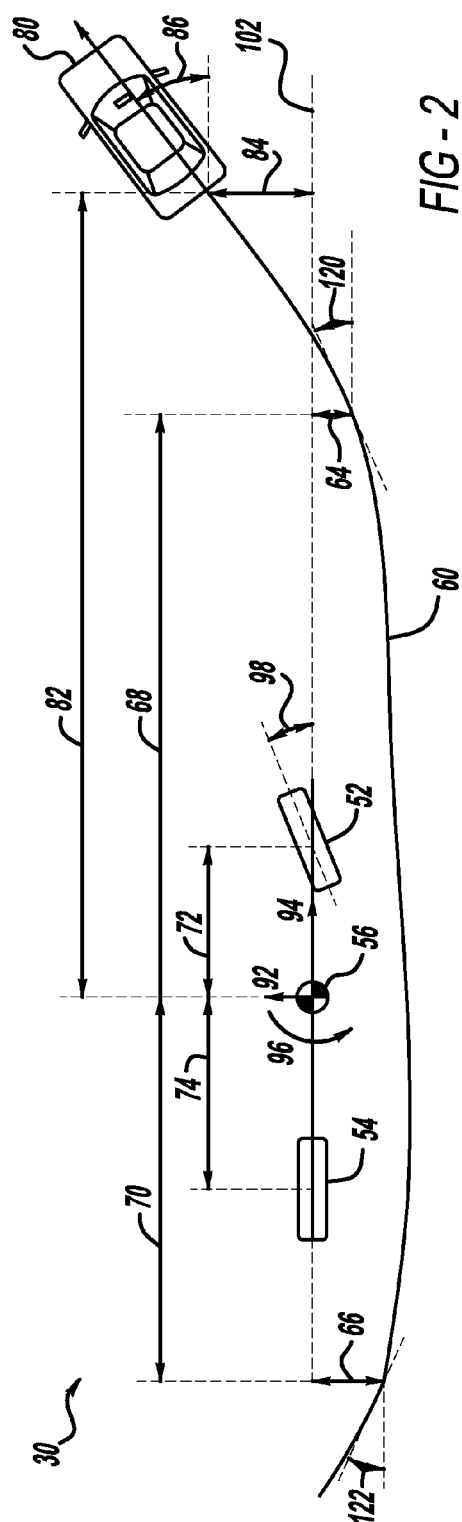
19 Claims, 6 Drawing Sheets

_10_

| 12 |
| 14 |
| 16 |
| 18 |

| 20 |

FIG - 1

_200_

| 12 |
| 14 |
| 16 |
| 18 |

| 210 |

| 220 |

FIG - 5

FIG - 2

FIG - 3

FIG - 4

FIG - 6

FIG - 7

FIG - 8

FIG - 9

FIG - 10
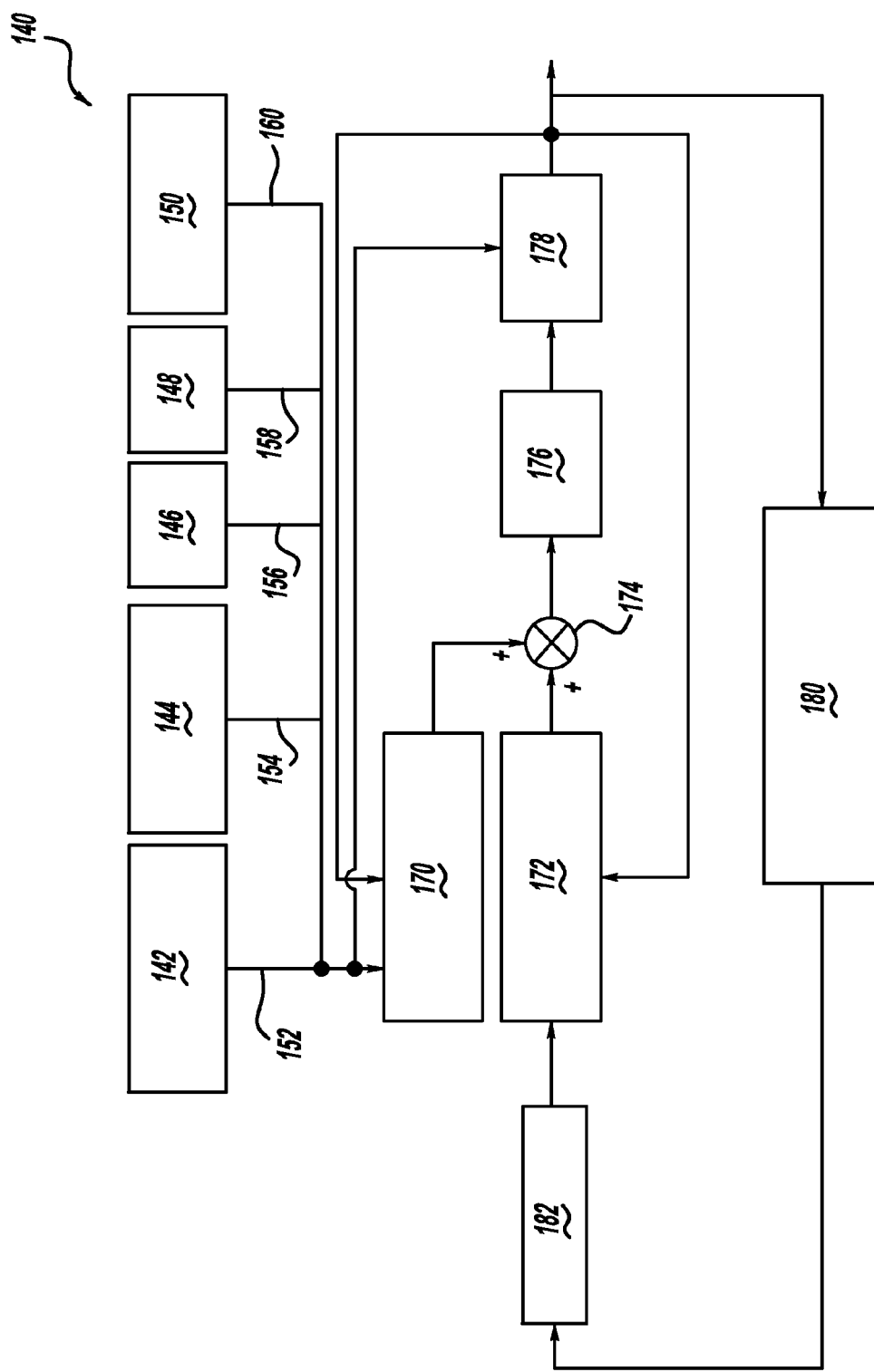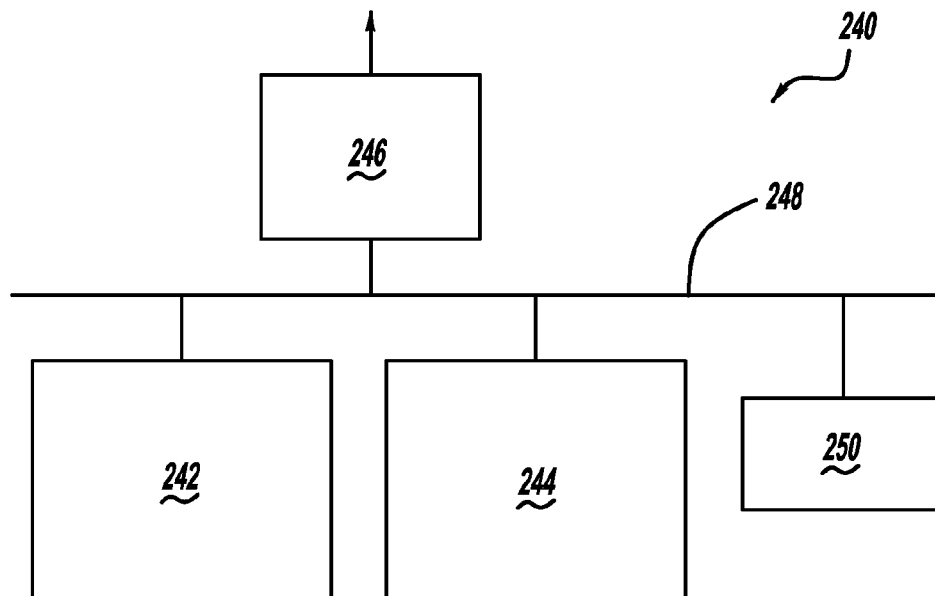
FIG - 11

LANE FUSION SYSTEM USING FORWARD-VIEW AND REAR-VIEW CAMERAS

BACKGROUND OF THE INVENTION

1. Field of the Invention

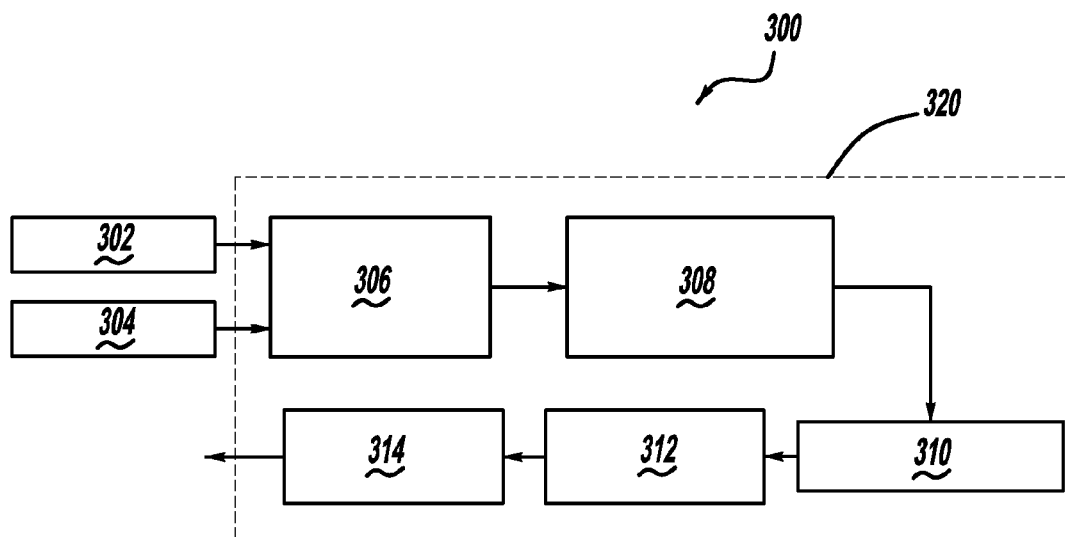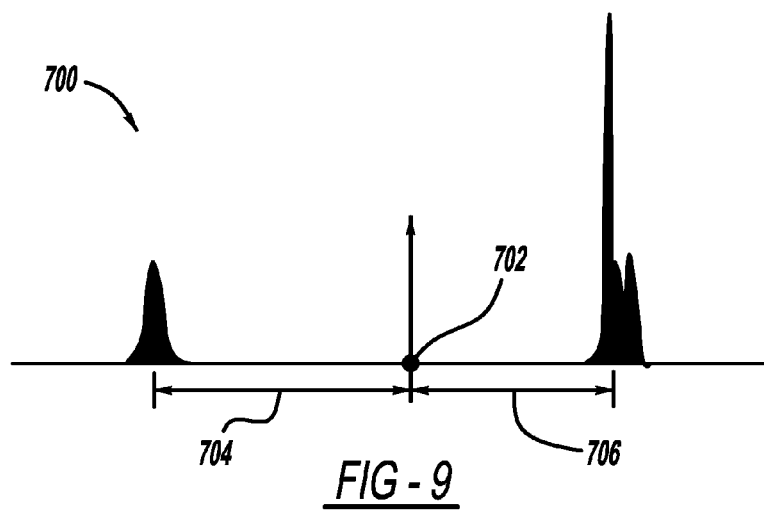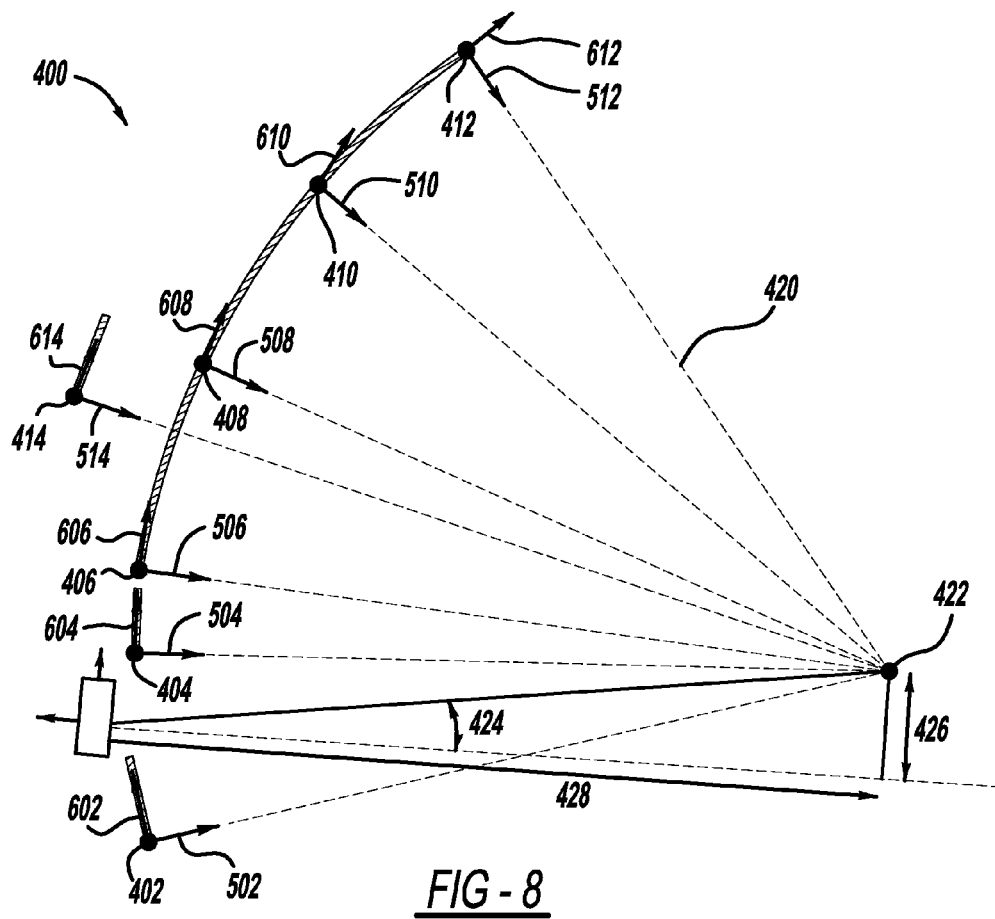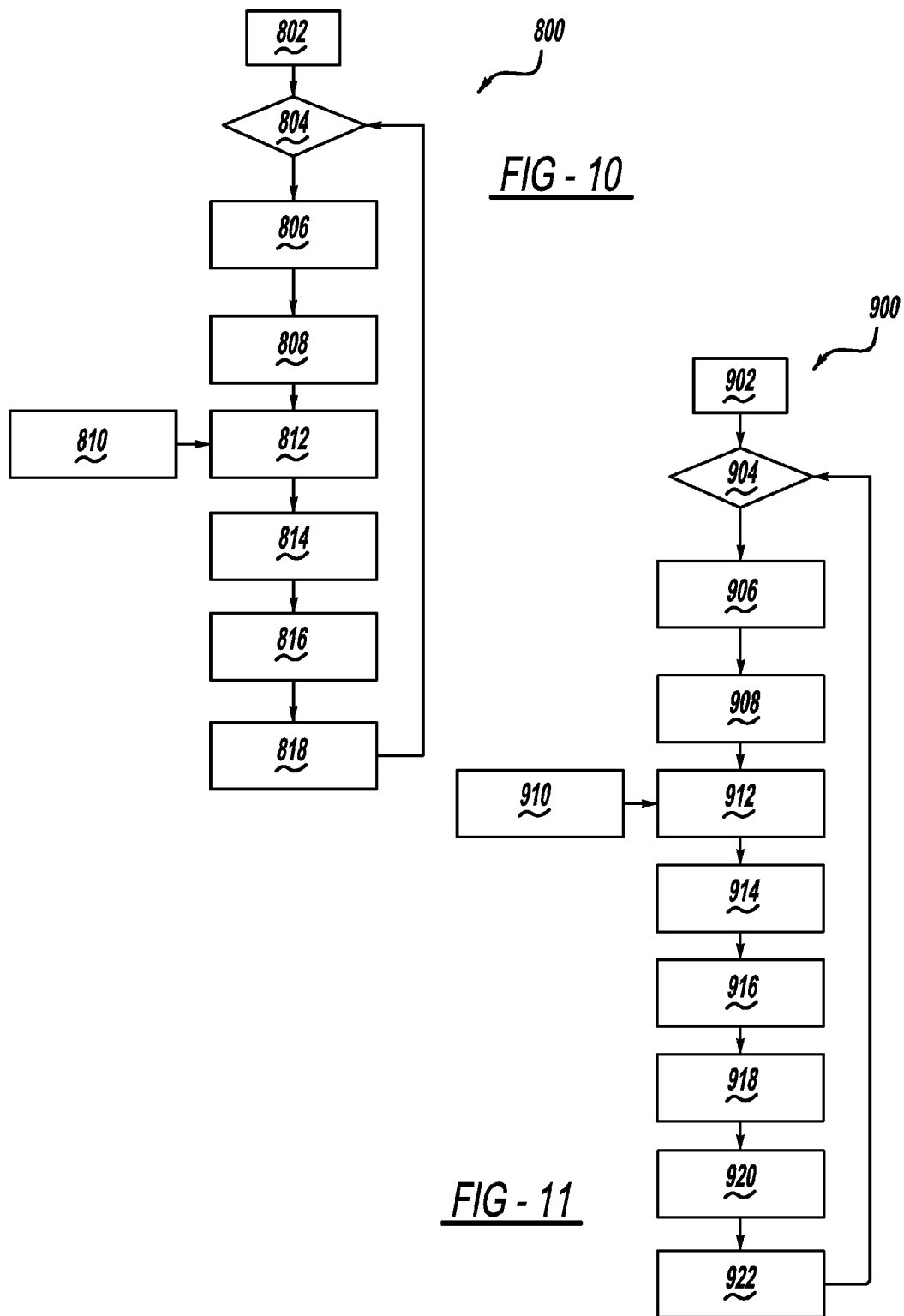This invention relates generally to a lane position method and system for a vehicle and, more particularly, to a lane position method and system for a host vehicle which uses a fusion of image data from forward-view and rear-view cameras and data from vehicle dynamics sensors to compute lane parameters, including lane curvature and the host vehicle's position and orientation relative to a lane reference path.

2. Discussion of the Related Art

Many modern vehicles include onboard cameras, which are used for a variety of purposes. One common application is a forward-viewing camera which can provide images to be used in a collision avoidance system, a lane departure warning system, a lateral control system, or a combination of these or other systems. However, conditions may arise which prevent a good image from being obtained from the forward-viewing camera. Such conditions include a leading vehicle at close range which blocks much of the camera's field of view, and low-visibility weather conditions, such as rain and fog, which obscure the camera's image. In such conditions, when a usable image from the forward-view camera is not available, systems which rely on the camera's image for input cannot be operated.

Meanwhile, many newer vehicles are also equipped with a rear-view camera, which is normally used only for backup assistance, such as providing a video image for the driver to see what is behind the vehicle. Although these rear-view cameras typically have a resolution and field of view which are more than sufficient for other image data collection purposes, until now they have not been used to supplement the images from forward-view cameras for lane position and lateral control applications.

There is an opportunity to use the image data available from a rear-view camera, and combine it with image data from a forward-view camera and other sensors, to provide a more robust lane sensing system. The resultant two-camera system not only makes use of more input data under normal conditions, but also provides a usable source of image data to allow operation of the system when conditions are unfavorable for forward-view imaging.

SUMMARY OF THE INVENTION

In accordance with the teachings of the present invention, a method and system are disclosed for computing lane curvature and a host vehicle's position and orientation relative to lane boundaries, using image data from forward-view and rear-view cameras and vehicle dynamics sensors as input. A host vehicle includes cameras at the front and rear, which can be used to detect lane boundaries such as curbs and lane stripes, among other purposes. The host vehicle also includes vehicle dynamics sensors including vehicle speed and yaw rate. A method is developed which computes lane curvature and the host vehicle's position relative to a lane reference path, where the lane reference path is derived from the lane boundaries extracted from a fusion of the front and rear camera images. Mathematical models provided in the disclosure include a Kalman filter tracking routine and a particle filter tracking routine.

Additional features of the present invention will become apparent from the following description and appended claims, taken in conjunction with the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a block diagram of a vehicle lateral control system which uses front and rear cameras and other sources of input;

FIG. 2 is a diagram of a bicycle model for lateral control of a host vehicle;

FIG. 3 is a diagram of the host vehicle showing many of the key parameters of the lateral control model;

FIG. 4 is a control block diagram showing how the vehicle lateral control model is implemented;

FIG. 5 is a block diagram of a system for vehicle lateral control using a 2-camera lane fusion approach;

FIG. 6 is a block diagram of a first embodiment of a lane fusion system using input from two cameras;

FIG. 7 is a block diagram of a second embodiment of a lane fusion system using input from two cameras;

FIG. 8 is a diagram which shows an example of lane stripe representation for a scenario where several short stripes and one long arc have been detected;

FIG. 9 is a histogram which shows how the displacement of the host vehicle to the lane boundaries can be computed;

FIG. 10 is a flow chart diagram of the Kalman filter tracking method used in the lane tracking module of FIG. 7; and

FIG. 11 is a flow chart diagram of the particle filter tracking method used in the lane tracking module of FIG. 7.

DETAILED DESCRIPTION OF THE EMBODIMENTS

The following discussion of the embodiments of the invention directed to a lane fusion system using forward-view and rear-view cameras is merely exemplary in nature, and is in no way intended to limit the invention or its applications or uses.

Many modern vehicles include forward-view cameras, and systems which use the image data from the forward-view cameras in applications such as lane departure warning and lateral control assistance. However, images from forward-view cameras can be obstructed by a leading vehicle, or obscured by sun glare, fog, rain, or snow, which reduces the reliability of applications which would rely on the images. Given the increasing availability of rear-view cameras, often used primarily for backup assistance, it makes sense to use the rear-view camera image data as a supplement to the forward-view camera image data. Along with GPS and digital map data, vehicle dynamics sensors, and radar-based or other systems capable of detecting a vehicle on the road ahead of the host vehicle, the forward-view and rear-view camera image data can be used in advanced applications for improved safety and vehicle control.

In one approach, the data sources are used directly in a vehicle lateral control application. FIG. 1 is a block diagram of a system 10 for lateral control of a vehicle using forward-view and rear-view cameras and other data sources. The system 10 uses image data from a forward-view camera 12 and a rear-view camera 14, as will be discussed below. A leading vehicle position system 16, which may be a long range radar (LRR) or other type system, tracks the position of a leading vehicle, for the purpose of estimating the path of the roadway. Road curvature information from a GPS-based navigation system or digital map 18 provides another source of data for the system 10. The inputs from the forward-view camera 12, the rear-view camera 14, the leading vehicle position system

16, and the digital map 18 are all used by a vehicle lateral control module 20, the operation of which will be discussed in detail below.

FIG. 2 is a diagram of a bicycle model 30 for vehicle lateral control, which is obtained by combining the two wheels of each axle into one wheel at the centerline of the vehicle. FIG. 3 is a diagram of a control model 40 which adds more detail to the bicycle model 30. Like elements and dimensions share the same reference numerals in FIGS. 2 and 3, which will be discussed together. The following table is provided as an index of the items and dimensions shown in FIGS. 2 and 3, including their reference numbers and descriptions.

Ref #	Symbol	Description
30	n/a	bicycle model
40	n/a	control model
50	n/a	host vehicle
52	n/a	front tire
54	n/a	rear tire
56	n/a	center of gravity point
60	n/a	lane reference path
62	κ	lane curvature
64	Δy_F	front lateral displacement
66	Δy_T	rear lateral displacement
68	d_F	longitudinal distance in front of center of gravity
70	d_T	longitudinal distance behind center of gravity
72	l_F	distance of front axle from center of gravity
74	l_T	distance of rear axle from center of gravity
80	n/a	leading target vehicle
82	X_O	forward distance of leading target vehicle from center of gravity of host vehicle
84	Y_O	lateral distance of leading target vehicle from center of gravity of host vehicle
86	θ_O	heading angle of leading target vehicle with respect to host vehicle
92	v_{yH}	host vehicle lateral velocity
94	v_{xH}	host vehicle longitudinal velocity
96	ω_H	host vehicle yaw rate
98	δ_F	front wheel steering angle
100	n/a	vehicle path
102	n/a	heading line
104	α_O	lateral offset between the heading line and the vehicle path at forward distance 82
106	ϵ_O	lateral offset between the vehicle path and the lane reference path at forward distance 82
108	α_F	lateral offset between the heading line and the vehicle path at forward distance 68
110	ϵ_F	lateral offset between the vehicle path and the lane reference path at forward distance 68
112	α_T	lateral offset between the heading line and the vehicle path at rearward distance 70
114	ϵ_T	lateral offset between the vehicle path and the lane reference path at rearward distance 70
120	θ_F	vehicle orientation angle with respect to tangent to lane reference path at forward distance 68
122	θ_T	vehicle orientation angle with respect to tangent to lane reference path at rearward distance 70

A host vehicle 50 is the subject of the bicycle model 30 and the control model 40, used in the vehicle lateral control module 20. The host vehicle 50 is represented by a front tire 52, a rear tire 54, and a center of gravity point 56 in the bicycle model 30. The host vehicle 50 is assumed to be equipped with a yaw rate sensor (not shown), and other sensors as necessary to know its longitudinal and lateral velocity.

A lane reference path 60 is assumed to be the centerline of a circular lane path with curvature κ, an estimate of which comes from the digital map 18. For the augmented lateral control system as considered in the bicycle model 30, the lateral displacement of the host vehicle 50 from the lane reference path 60 is measured both as a front lateral displacement Δy_F and a tail lateral displacement Δy_T by the forward-view camera 12 and the rear-view camera 14, respectively.

The displacement measurements are acquired by the cameras at a longitudinal distance d_F in front of the center of gravity point 56 and a distance d_T behind the center of gravity point 56. The distances d_F and d_T are time variant and dependent on the quality of lane markers detected by the cameras 12 and 14, occlusion by leading or following vehicles, and lighting conditions.

The leading vehicle position system 16 onboard the host vehicle 50 can detect a leading target vehicle 80, and provide its longitudinal distance X_O, lateral distance Y_O, and heading angle θ_O. Only a vehicle immediately in front of the host vehicle 50 and within a distance threshold (e.g., 50 m) is considered as the leading target vehicle 80. Other vehicle parameters in the bicycle model 30 are distances l_F and l_T of the front and rear axles, respectively, from the center of gravity point 56. Three host vehicle state variables are also shown: vehicle lateral velocity v_{yH} vehicle longitudinal velocity v_{xH}, and vehicle yaw rate ω_H. A front wheel steering angle δ_F is the input of the automatic steering system as commanded by the lateral control system 20.

A vehicle path 100 describes the path the host vehicle 50 is currently following, and a heading line 102 represents a straight line through the centerline of the host vehicle 50. Distance α_O is the lateral offset between the heading line 102 and the vehicle path 100 at the forward distance X_O. Distance ϵ_O is the lateral offset between the vehicle path 100 and the lane reference path 60 at the forward distance X_O. Distance α_F is the lateral offset between the heading line 102 and the vehicle path 100 at the forward distance d_F. Distance ϵ_F is the lateral offset between the vehicle path 100 and the lane reference path 60 at the forward distance d_F. Distance α_T is the lateral offset between the heading line 102 and the vehicle path 100 at the rearward distance d_T. Distance ϵ_T is the lateral offset between the vehicle path 100 and the lane reference path 60 at the rearward distance of d_T.

Vehicle orientation with respect to the lane reference path tangent at the forward distance d_F is represented by angle θ_F, and vehicle orientation with respect to the lane reference path tangent at the rearward distance d_T is represented by angle θ_T.

In addition to the elements and dimensions shown in the bicycle model 30 and the control model 40, the following symbols must also be defined: m=Total mass of the host vehicle 50; I_ω=Total inertia of the host vehicle 50 around the center of gravity point 56; l=Distance between the front and rear axles, ($l=l_F+l_T$); and c_F, c_T=Cornering stiffness of the front and rear tires, 52 and 54, respectively.

A linearized bicycle state-space model of the lateral vehicle dynamics can be written as:

$$\begin{bmatrix} \dot{v}_{yH} \\ \dot{\omega}_H \end{bmatrix} = \begin{bmatrix} -\dfrac{c_F + c_T}{m v_{xH}} & \dfrac{c_T l_T - c_F l_F}{m v_{xH}} - v_{xH} \\ \dfrac{-l_F c_F + l_T c_T}{I_\omega v_{xH}} & -\dfrac{l_F^2 c_F + l_T^2 c_T}{I_\omega v_{xH}} \end{bmatrix} \begin{bmatrix} v_{yH} \\ \omega_H \end{bmatrix} + \begin{bmatrix} \dfrac{c_F}{m} \\ \dfrac{l_F c_F}{I_\omega} \end{bmatrix} \delta_F \tag{1}$$

The state-space equations capturing the evolution of the forward-view camera measurements due to the motion of the host vehicle 50 and changes in the road geometry are:

$$\Delta \dot{y}_F = v_{xH} \theta_F - v_{yH} - \omega_H d_F \tag{2}$$

$$\dot{\theta}_F = v_{xH} \kappa - \omega_H \tag{3}$$

Similarly, the state-space equations capturing the evolution of the rear-view camera measurements due to the motion of the host vehicle 50 and changes in the road geometry are:

$$\Delta \dot{y}_T = v_{xH} \theta_T - v_{yH} + \omega_H d_T \tag{4}$$

$$\dot{\theta}_T = v_{xH} \kappa - \omega_H \tag{5}$$

It is assumed that the leading target vehicle **80** is following the centerline of the lane reference path **60**, thus the state-space equations capturing the evolution of the radar measurements due to the motion of the host vehicle **50** and changes in the road geometry are:

$$\dot{Y}_O = v_{xH}\theta_O - v_{yH} - \omega_H X_O \tag{6}$$

$$\dot{\theta}_O = v_{xH}\kappa - \omega_H \tag{7}$$

The vehicle lateral dynamics, front camera dynamics, rear camera dynamics, and leading target vehicle dynamics described in Equations (1)-(7) can then be combined into a single dynamic system of the form:

$$
\begin{bmatrix}
\dot{v}_{yH} \\
\dot{\omega}_H \\
\Delta\dot{y}_F \\
\dot{\theta}_F \\
\Delta\dot{y}_T \\
\dot{\theta}_T \\
\dot{Y}_O \\
\dot{\theta}_O
\end{bmatrix}
=
\begin{bmatrix}
-\dfrac{c_F+c_T}{mv_{xH}} & \dfrac{c_T l_T - c_F l_F}{mv_{xH}} - v_{xH} & 0 & 0 & 0 & 0 & 0 & 0 \\
\dfrac{-l_F c_F + l_T c_T}{I_\omega v_{xH}} & -\dfrac{l_F^2 c_F + l_T^2 c_T}{I_\omega v_{xH}} & 0 & 0 & 0 & 0 & 0 & 0 \\
-1 & -d_F & 0 & v_{xH} & 0 & 0 & 0 & 0 \\
0 & -1 & 0 & 0 & 0 & 0 & 0 & 0 \\
-1 & d_T & 0 & 0 & 0 & v_{xH} & 0 & 0 \\
0 & -1 & 0 & 0 & 0 & 0 & 0 & 0 \\
-1 & -X_O & 0 & 0 & 0 & 0 & 0 & v_{xH} \\
0 & -1 & 0 & 0 & 0 & 0 & 0 & 0
\end{bmatrix}
$$

$$
\begin{bmatrix}
v_{yH} \\
\omega_H \\
\Delta y_F \\
\theta_F \\
\Delta y_T \\
\theta_T \\
Y_O \\
\theta_O
\end{bmatrix}
+
\begin{bmatrix}
\dfrac{c_F}{m} \\
\dfrac{l_F c_F}{I_\omega} \\
0 \\
0 \\
0 \\
0 \\
0 \\
0
\end{bmatrix}
\delta_F
+
\begin{bmatrix}
0 \\
0 \\
0 \\
v_{xH}\kappa \\
0 \\
v_{xH}\kappa \\
0 \\
v_{xH}\kappa
\end{bmatrix}
$$

or in short as:

$$\dot{x} = f(x) + g(\delta_F) \tag{8}$$

Let $y = [\dot{\omega}_H\ \Delta\dot{y}_F\ \dot{\theta}_F\ \Delta\dot{y}_T\ \dot{\theta}_T\ \dot{Y}_O\ \dot{\theta}_O]^T$ denote the output of the dynamic system, observed by the yaw rate sensor, the forward-view camera **12**, the rear-view camera **14**, and the leading vehicle position system **16**. The observation equation can be written as $y = o(x)$.

Referring to the lane reference path **60** and the vehicle path **100** of FIG. **3**, the goal of the lateral control module **20** is to track the roadway by regulating the lateral differences between the lane reference path **60** (i.e., Δy_F, Δy_T and Y_O) and the vehicle path **100** (i.e., α_F, α_T, and α_O) at distances of d_F, d_T, and X_O, measured by the forward-view camera **12**, the rear-view camera **14**, and the leading vehicle position system **16**, respectively. Namely, the control objective is to minimize:

$$J = w_F\epsilon_F - w_T\epsilon_T + w_O\epsilon_O \tag{9}$$

where $\epsilon_F = \Delta y_F - \alpha_F$, $\epsilon_T = \Delta y_T - \alpha_T$, and $\epsilon_O = Y_O - \alpha_O$; and w_F, w_T, and w_O are normalized positive weights such that $w_F + w_T + w_O = 1$.

Equation (9) can then be written as:

$$J = h(x) \tag{10}$$

Feedback linearization is a common approach used in controlling nonlinear system. The approach involves coming up with a transformation of the nonlinear system into an equiva-

lent linear system through a change of variables and a suitable control input. The application of this technique to the bicycle model **30** is not linearization since the bicycle model **30** is already linear. But this technique can be applied to render the bicycle model **30** independent of the host vehicle longitudinal velocity v_{xH}.

The control law required to linearize the system expressed in Equations (8) and (10) by differentiating Equation (10) twice with respect to time is as follows:

$$\delta_F = \frac{1}{L_g L_f^2 h(x)}(-L_f^2 h(x) + u) \tag{11}$$

where L_f^i denotes the i-th Lie derivative along function f. A Lie derivative evaluates the change of one vector field along the flow of another vector field, as is known to those skilled in the art of mathematics.

Employing this control law yields a second order equation of the form $\ddot{J} = u$. Let $z_1 = J$. The resulting simplified dynamic system can be expressed as:

$$\dot{z}_1 = z_2$$

$$\dot{z}_2 = u \tag{12}$$

Using the following state feedback control law:

$$u = -k_1 z_1 - k_2 z_2 \tag{13}$$

the second order system Equation (12) can be written as $\dot{z} = Az$, with

$$A = \begin{bmatrix} 0 & 1 \\ k_1 & k_2 \end{bmatrix}.$$

Therefore, with appropriate choice of k_1 and k_2, a stable lane tracking system can be designed with the eigenvector of A in the open left half of the complex plane.

As shown in FIG. **1**, the digital map **18** provides input to the lateral control module **20**, including an estimate of the lane curvature κ, which can be used as part of a feed-forward control strategy. By letting $[\dot{v}_{yH}\ \dot{\omega}_H\ \Delta\dot{y}_F\ \dot{\theta}_F]^T = 0$, the steering input, δ_{fwd}, that tracks a lane curvature κ can be computed from Equations (1)-(3) as:

$$\delta_{fwd} = \kappa\left(l - \frac{(l_F c_F - l_T c_T)v_{xH}^2 m}{c_T c_F l}\right) \tag{14}$$

This feed-forward component of Equation (14) can be added to the above derived control law in Equations (11) and (13) to improve the transient behavior of the host vehicle **50** when entering and exiting curves.

FIG. **4** is a control block diagram **140** which shows how the vehicle lateral control strategy described above is implemented. The steps in the control method are outlined as follows:

1) At box **142**, the digital map **18** provides an estimate of the lane curvature κ on line **152**.
2) At box **144**, vehicle dynamics sensors provide the vehicle forward velocity v_{xH} and yaw rate ω_H measurements on line **154**.
3) At box **146**, the forward-view camera **12** provides measurements of the lane orientation θ_F, the lateral displace-

ment Δy_F, and the longitudinal distance where the measurement is taken d_F, on line **156**.

4) At box **148**, the rear-view camera **14** provides measurements of the lane orientation θ_T, the lateral displacement Δy_T, and the longitudinal distance where the measurement is taken d_T, on line **158**.

5) At box **150**, the leading vehicle position system **16** provides leading target vehicle position, i.e., the longitudinal offset X_O, the lateral offset Y_O, and the heading θ_O, on line **160**.

6) The inputs on the lines **152-160** are provided to box **170**, where the feed-forward term δ_{fwd} is computed as in Equation (14).

7) At box **172**, the feedback linearization term δ_F, is computed as in Equation (11).

8) At summing junction **174**, the feed-forward term δ_{fwd} and the feedback linearization term δ_F, are added together, and sent to a steering actuator (electric power steering, or other type system) in the host vehicle **50** at box **176**.

9) At box **178**, an Observer module estimates the vehicle's state variables using a Kalman filter, with the data on the lines **152-160** and the vehicle's response as inputs, using Equation (8) and y=o(x).

10) At box **180**, a variable change module computes z_1 and z_2 using Equations (10) and (12).

11) At box **182**, the feedback term u is computed for the linearized dynamic system using Equation (12).

Some examples are provided to further explain the operation of the control method described above. In the best case scenario, measurements from all three external sensors are available; that is, rearward lane boundary information from the rear-view camera **14**, forward lane boundary information from the forward-view camera **12**, and leading vehicle information from the leading vehicle position system **16**. In such a case, the weight parameters in Equation (9) are defined to be proportional to the quality of the measurement (i.e., signal-noise ratio, or variance of the estimates) returned by the corresponding sensors. For example, let measurement variances of the forward-view camera **12**, the rear-view camera **14**, and the leading vehicle position system **16** be σ_F, σ_T, and σ_O, respectively. Then the corresponding weights are computed as:

$$w_F = Ce^{-\frac{\sigma_F^2}{W}}, \; w_T = Ce^{-\frac{\sigma_T^2}{W}}, \; w_O = Ce^{-\frac{\sigma_O^2}{W}} \tag{15}$$

where C is the normalization parameter such that $w_F+w_T+w_O=1$, and W is a bandwidth parameter chosen by the designer.

In a situation where the leading target vehicle **80** blocks the view of the forward-view camera **12**, such that little or no forward lane boundary information is available, the weight parameters of Equation (9) would be tuned by decreasing the value of w_F (possibly to zero), and increasing the values of w_T and w_O. Similarly, in a situation where there is no suitable leading target vehicle **80**, the value of w_O would be set to zero, and the values of w_F and w_T would be increased. Finally, in a situation where a low-angle sun or inclement weather obscures the image from the forward-view camera **12**, such that no forward lane boundary information is available, the weight parameters of Equation (9) would be tuned by setting the value of w_F to zero, and increasing the values of w_T and w_O.

Using the control method described above, a robust vehicle lateral control system can be implemented. By directly using front and rear camera images as input, along with other indicators of road curvature, the lateral control system can pro-

vide more reliable and stable performance than lateral control systems which do not use as many sources of input.

Another approach to vehicular lateral control can be achieved by first combining the data from the forward-view camera **12** and the rear-view camera **14** in a data fusion module, and then using the resultant lane curvature and displacement information from the fusion module in a lateral control module.

FIG. **5** is a block diagram of a system **200** for vehicle lateral control using a 2-camera lane fusion approach. Like the system **10** shown in FIG. **1**, the system **200** uses data from the forward-view camera **12**, the rear-view camera **14**, the leading vehicle position system **16**, and the digital map **18**. However, unlike the system **10** which uses the inputs directly in the lateral control module **20**, the system **200** first combines the inputs in a data fusion module **210**. The outputs of the data fusion module **210**, including roadway curvature, and the vehicle's displacement and orientation relative to lane boundaries, are then provided to a vehicle lateral control module **220**. The outputs of the data fusion module **210** may also be used in applications other than a lateral control system, such as a lane departure warning system.

Two methods of performing lane data fusion will be discussed below. In this discussion, many of the variables and dimensions from FIGS. **2** and **3** will be referenced.

A traditional lane information system with lane departure warning typically includes the forward-view camera **12** that can measure the vehicle orientation with respect to the tangent of the lane θ_F at the front, the front lateral displacement Δy_F at the front bumper, and the lane curvature κ, where the distance d_F is defined as the distance from the center of gravity point **56** to the front bumper of the host vehicle **50**. Besides the functionality providing backup assistance, the rear-view camera **14** can offer additional lane sensing measurements; the vehicle orientation with respect to the tangent of the lane θ_T at the rear, and the rear lateral displacement Δy_T at the rear bumper, where the distance d_T is defined as the distance from the center of gravity point **56** to the rear bumper of the host vehicle **50**. The two additional camera measurements, θ_T and Δy_T, are valuable in design of a robust fusion system for lane sensing. They are especially useful in inclement weather and lighting conditions, such as front low-angle sun, partially snow-covered lane markers, reduced visibility due to fog, and the like, where the quality of images from the forward-view camera **12** would be reduced.

FIG. **6** is a block diagram of a first embodiment of a lane fusion system **240** using input from two cameras. In the system **240**, a full-fledged forward lane sensor system **242** and a full-fledged rear lane sensor system **244** each include a camera and a processor, and can detect and track lane boundaries at their respective ends of the host vehicle **50**. The forward lane sensor system **242** and the rear lane sensor system **244** provide their measurements to a lane fusion module **246** which computes enhanced lane boundary and orientation information. The forward lane sensor system **242** sends measurements θ_F, Δy_F, and κ to the fusion module **246** at a fixed sample rate (e.g., 10 Hz). The rear lane sensor system **244** sends measurements θ_T and Δy_T at the same fixed sample rate. The forward lane sensor system **242**, the rear lane sensor system **244**, and the fusion module **246** are interconnected by a serial network **248**, which may use the Control Area Network (CAN) or other protocol.

The fusion module **246** takes inputs from both the front and rear lane sensor systems **242** and **244**, and vehicle dynamic sensors **250**, and outputs the enhanced lane information: vehicle orientation with respect to the tangent of the lane (θ), displacement of the front bumper center to the lane boundaries (Δy), and the lane curvature (κ). As mentioned previously, the lane information could be used by various downstream applications.

Let the measurements from the vehicle dynamic sensors **250** include vehicle speed (v_H) and yaw rate (ω_H). Then the following Kalman filter is designed to fuse the information from both the front and rear lane sensor systems **242** and **244**.

Let the state variables be $s=(\kappa, \theta, \Delta y, \phi_F, \phi_T)$, where κ, θ and Δy are defined as above; and ϕ_F and ϕ_T are the azimuth misalignment of the front and rear lane systems **242** and **244**, respectively.

The state dynamic equation is written as:

$$\kappa'=\kappa+v_\kappa$$

$$\theta'=\theta-\omega_H\Delta T+\kappa v_H\Delta T+v_\theta$$

$$\Delta y'=\Delta y+v_H\Delta T\theta+v_{\Delta y}$$

$$\phi'_F=\phi_F$$

$$\phi'_R=\phi_R \tag{16}$$

or in short as:

$$s'=Fs+u+Gv \tag{17}$$

where $v=(v_\kappa, v_\theta, v_{\Delta y})^T$ denotes a zero-mean Gaussian white noise vector modeling the uncertainty of the state dynamics model;

$$F = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 \\ v_H\Delta T & 1 & 0 & 0 & 0 \\ 0 & v_H\Delta T & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 1 \end{bmatrix}, u = [0 \quad -\omega_H\Delta T \quad 0 \quad 0 \quad 0]^T,$$

$$\text{and } G = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 \end{bmatrix}.$$

The measurement model can be written as:

$$\theta_F\theta+\phi_F+w_{\theta_F}$$

$$\Delta y_F=\Delta y+w_{\Delta y_F}$$

$$\kappa_F=\kappa+w_\kappa$$

$$\theta_T=\theta+\phi_T+w_{\theta_T}$$

$$\Delta y_T=\Delta y+w_{\Delta y_t} \tag{18}$$

or in short as:

$$o = Hs + w \tag{19}$$

$$\text{where } H = \begin{bmatrix} 0 & 1 & 0 & 1 & 0 \\ 0 & 0 & 1 & 0 & 0 \\ 1 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0 & 0 \end{bmatrix},$$

$o=[\theta_F \, \Delta y_F \, \kappa_F \, \theta_T \, \Delta y_T]^T$, and $w=[w_{\theta_F} \, w_{\Delta y_F} \, w_\kappa \, w_{\theta_T} \, w_{\Delta y_T}]^T$ is a zero-mean Gaussian white noise vector modeling the quality of the measurements from the front and rear lane sensor systems **242** and **244**.

In summary, the following Kalman filtering procedure jointly estimates the misalignment angles and the lane parameters:

1) Randomly choose small numbers to initialize the misalignment parameters $\phi_F(0)$ and $\phi_T(0)$; combining the misalignment parameters with the first measurement from the front lane sensor **242** yields $s(0)=(\kappa_F(0), \theta_F(0), \Delta y_F(0), \phi_F(0), \phi_T,(0))^T$, and a covariance matrix $P(0)$ is chosen for $s(0)$.

2) When the new measurement at time instant t arrives, the previous state vector is written as $s(t-1)$; the predicted state at time instant t can be written as $\tilde{s}(t)=Fs(t-1)+u(t)$, and the covariance matrix $\tilde{P}(t)=P(t-1)+GQG^T$, where Q is the covariance matrix of the noise vector v.

3) Let the measurement at time instant t be o; thus the updated state vector at time instant t is:

$$e=o-h(\tilde{s}(t))$$

$$S=H\tilde{P}(t)H^T+R$$

$$K=\tilde{P}(t)H^TS^{-1}$$

$$\hat{s}(t)=\tilde{s}(t)+Ke$$

$$P(t)=(I-KH_t)\tilde{P}(t)$$

where R is the covariance matrix.

4) Output $\hat{s}(t)$ as the fusion output.

5) Go to Step 2.

Using the above procedure, the fusion module **246** of the system **240** computes a combined set of lane parameters for the host vehicle **50**, while simultaneously determining the misalignment parameters for the front and rear lane sensor systems **242** and **244**.

FIG. **7** is a block diagram of a second embodiment of a lane fusion system **300** using input from two cameras. The system **300** does not include full-fledged lane sensor systems at the front and rear. Instead, the system **300** includes a forward-view camera **302** and a rear-view camera **304**. The cameras **302** and **304** only capture images and send them to a fusion module **320**, which combines both images together, detects and tracks the lane markers.

Images from the forward-view and rear-view cameras **302** and **304**, respectively, are provided to box **306** to find local high intensity regions. The key idea of the box **306** is to find stable local high-intensity regions in different spatial scales. The algorithm begins with building a Gaussian pyramid. At each pyramid scale, the image is subtracted by the enlarged coarse-level image, which is further blurred. Then the local maximum finding operation is applied to the difference images at different scales, and all maxima whose height is less than a threshold h are suppressed. Thus the binary images of possible lane markers are derived at the box **306**.

At box **308**, the detected pixels of curbs and stripes are projected onto ground plane in the vehicle coordinate system based on the camera calibration parameters. At box **310**, point clouds of the projected pixels from the box **308** are first clustered based on the similarity measure (distance). Close pixels are clustered into a single component. Then the components are classified based on their geometry shape. Components whose shape matches with curbs and lane stripes are selected, and then line fitting and arc fitting procedures are applied to fit the stripe candidates. The components whose shape do not match with a line or an arc are discarded.

At box **312**, the fitted stripes in vehicle coordinate system are then linked into a lane boundary. At box **314**, lane information is tracked and output. This includes: monitoring the fitted stripes and data from vehicle dynamic sensors; tracking

the lane boundary; and estimating lane information, including the lane curvature (κ), the vehicle orientation with respect to the tangent of the lane (θ), and the displacement of the front bumper center to the lane boundaries (Δy). Details of the algorithms used in the boxes **308-314** are given below.

The projection algorithm of the box **308** requires the following camera intrinsic parameters:

Focal length: The focal length in pixels, [f_u, f_v];

Optical center: [c_u, c_v];

Skew coefficient: The skew coefficient defining the angle between the x and y pixel axes is stored in the scalar α_c;

Distortions: The image distortion coefficients (radial and tangential distortions) are stored in the vector $k_c=(k_1, k_2, k_3, k_4, p_1, p_2)$, where ($k_1, k_2, k_3, k_4$) is radial distortion coefficients and (p_1, p_2) is tangential coefficients;

and camera extrinsic parameters:

Translation vector T;

Rotation matrix R;

The camera extrinsic parameters are estimated through a camera calibration process, many of which are known in the art, and which need not be discussed here.

An iterative procedure used to remove the distortion is outlined below. The input includes a set of pixels S={(u_i, v_i)|i=1, . . . , N} and the above-defined camera intrinsic parameters. The output is the rectified set of pixels S'={(u'_i, v'_i)|i=1, . . . , N}. The procedure is as follows:

1) For each pixel $s_i=(u_i, v_i)$, i=1, . . . N;

2) Iteratively execute the following steps 20 times:

a. Let

$$u = \begin{bmatrix} u_i \\ v_i \end{bmatrix}$$

and r=||x||.

b. Compute radial correction:

$$k_{rad}=1+k_1 r+k_2 r^2+k_3 r^3+k_4 r^4.$$

c. Compute tangential correction:

$$\Delta u = \begin{bmatrix} 2p_1 u_i v_i + p_2(r^2 + 2u_i^2) \\ p_1(r^2 + 2v_i^2) + 2p_2 u_i v_i \end{bmatrix}.$$

d. Correct the pixel $u=(u+\Delta u)/k_{rad}$.

3) Output u as the final corrected pixel (u'_i, v'_i).

After the above rectification, or distortion removing process, the following transformation can be applied. The input includes a set of rectified pixels S'={(u'_i, v'_i)|i=1, . . . , N} and the camera extrinsic parameters described above. The output is the detected lane marker points projected onto the vehicle frame: X={(x_i, y_i)|i=1, . . . N}. The transformation process is as follows:

1) For each pixel $s_i=(u_i, v_i)$, i=1, . . . , N;

a. Let $u = \begin{bmatrix} u'_i \\ v'_i \end{bmatrix}$ and $K_K = \begin{bmatrix} f_u & \alpha_c f_u & c_u \\ 0 & f_v & c_v \\ 0 & 0 & 1 \end{bmatrix}$.

b. Compute P=K_k[R T].

c. Let H=[p_1 p_2 p_4] where p_j, j=1, . . . , 4 is the column vector.

d. Compute z=$H^{-1}u$.

2) Output z as the projected pixel (x_i, y_i) in ground plane in vehicle frame.

The above rectification and transformation procedures are applied at the box **308** to provide a set of highlighted pixels, that is, points that are candidate curb or lane stripe points, in the vehicle coordinate frame. Then, at the box **310**, the pixels

or points are clustered together into curbs and lane stripes. Given the lane marker pixel set

$$X = \left\{ z_i \mid z_i = \begin{bmatrix} x_i \\ y_i \end{bmatrix} \right\},$$

i=1, . . . N}, the pixels are first clustered into stripes and then the stripes are fit into line or arc segments.

First, in order to cluster adjacent pixels into a stripe, a similarity graph G=(V, E) is constructed where the vertex set is defined as the pixels on ground, i.e., V={z_i|i=1, . . . N} and the edge set E is defined as a set of pixel pairs if each pixel pair's distance on the ground plane is less than a threshold (T_{sep}), or each pixel pair is in 8-neighbor proximity of each other in the image plane, i.e., E={(z_i,z_j)|||z_i−z_j||<T_{sep} ∨ Neighbor(s_i,s_j)}, where s_i and s_j are the corresponding locations in the image plane; and Neighbor(s_i,s_j) is true if s_i and s_j are in 8-neighbor proximity of each other. In this clustering methodology, 8-neighbor proximity means that a second pixel is one of the 8 nearest neighbors (immediately left, right, above, below, above-left, above-right, below-left, or below-right) of a first pixel, in an approximately rectangular grid of pixels.

Next a depth-first search (DFS) strategy is applied to partition the graph into connected components: {X_1, . . . , X_c}. Then each of the clustered stripes is fitted with a line or an arc.

Let $z_i=(x_i, y_i)$, i=1 . . . , N_c be a pixel in a detected stripe. The stripe can be fitted by a line parametric equation (Ax+By=d, such that $A^2+B^2=1$). The parameters A, B and d can be estimated via least-squares, such as minimizing:

$$\|D\beta\|^2, D = \begin{pmatrix} x_1 & y_2 & 1 \\ x_2 & y_2 & 1 \\ \vdots & \vdots & \vdots \\ x_{N_c} & y_{N_c} & 1 \end{pmatrix}, \beta = \begin{pmatrix} A \\ B \\ d \end{pmatrix} \quad (20)$$

which can be solved by finding the eigenvector of X with the smallest eigenvalue λ_m:

$$D\beta=\lambda_m\beta \quad (21)$$

The fitting residue is defined as e=λ_m.

The width W and length L of the stripe are computed as:

$$W = \max_i (z_i^T n) - \min_i (z_i^T n), L = \max_i (z_i^T t) - \min_i (z_i^T) \quad (22)$$

respectively, where n and t are the normal and tangential vectors (unit length) of the line segment, i.e.,

$$n = \begin{bmatrix} \frac{A}{r} & \frac{B}{r} \end{bmatrix} \text{ and } d' = \frac{d}{r} \text{ with } r = \sqrt{A^2 + B^2}.$$

Then t is derived by rotating n by 90 degrees.

The two endpoints of the stripe are:

$$e_s = z_m - (n^T z_m - d)'n \quad (23)$$

$$e_e = z_M - (n^T z_M - d)'n$$

where indices $m = \underset{i=1,\dots,N_c}{\operatorname{argmin}} (z_i^T t)$ and $M = \underset{i,1,\dots,N_c}{\operatorname{argmax}} (z_i^T t)$.

The orientation (angle) of the stripe is ϕ=a tan 2 (A, B).

If the residue of line fitting is larger than a threshold, the stripe is fit again using a circle parametric equation (x^2+y^2+

$a_1x + a_2y + a_3 = 0$). The parameters a_1, a_2, and a_3 can be estimated via least-squares, such as minimizing:

$$\|C\alpha - b\|^2, \quad C = \begin{bmatrix} x_1 & y_1 & 1 \\ x_2 & y_2 & 1 \\ \vdots & \vdots & \vdots \\ x_{N_c} & y_{N_c} & 1 \end{bmatrix}, \tag{24}$$

$$b = \begin{bmatrix} -(x_1^2 + y_1^2) \\ -(x_2^2 + y_2^2) \\ \vdots \\ -(x_{N_c}^2 + y_{N_c}^2) \end{bmatrix}, \quad \alpha = \begin{bmatrix} a_1 \\ a_2 \\ a_3 \end{bmatrix}$$

with respect to α.

The solution of the above least squares is $\alpha = (C^TC)^{-1}C^Tb$. The radius and center of the fitted circle can be written as:

$$R = (a_1^2 + a_2^2)/4 - a_3 \tag{25}$$

$$x_c = -\frac{a_1}{2}$$

$$y_c = -\frac{a_2}{2}$$

respectively.

The two endpoints of the fitted arc can be computed as:

$$e_s = [x_c + R \cos \phi_m, y_c + R \sin \phi_m]^T$$

$$e_e = [x_c + R \cos \phi_M, y_c + R \sin \phi_M]^T \tag{26}$$

and the stripe's orientation (angle) at the endpoints are $\phi_s = \phi_m$ and $\phi_e = \phi_M$, where the indices

$$m = \underset{i=1,\ldots,N_c}{\mathrm{argmin}}(\mathrm{atan}(y_i - y_c, x_i - x_c))$$

and

$$M = \underset{i=1,\ldots,N_c}{\mathrm{argmax}}(\mathrm{atan}(y_i - y_c, x_i - x_c)).$$

The width W and length L of the stripe are computed as follows:

$$W = \max(\|z_i - c\|) - \min(\|z_i - c\|) \tag{27}$$

and

$$L = \|e_s - e_e\| \tag{28}$$

respectively, where $c = [x_c \; y_c]^T$ denotes the center of the circle.

In summary, the output of the box **310** is a list of stripes fitted with line segments with the following parameters; normal vector (n), distance to the origin (d'), width (W), length (L), orientation (ϕ), and start points (e_s); or arc segments with the following parameters; the center of the circle (c), radius (R), width (W), length (L), and two end points' positions (e_s and e_e).

FIG. **8** is a diagram **400** which shows an example of lane stripe representation for a scenario where the following have been detected: line segment #**1** represented by end point **402** and normal vector **502**, line segment #**2** (**404**, **504**), line segment #**3** (**414**, **514**), and arc segment with radius **420**, center (c) **422**, first end point **406**, and second end point **412**.

The following steps are used at the box **312** to link the stripes into left and right lane boundaries.

First, any stripe whose aspect ratio (L/W) is less than a threshold is removed. Only slim stripes are kept for further processing. Then long arc or line segments are broken down into short segments, and each segment is represented by a start end point (e) and a tangential vector (t). For example, in the diagram **400**, the start end point and tangential vector for line segment #**1** are represented as (**402, 602**); and the long arc is broken up into four end points: (**406, 606**), (**408, 608**), (**410, 610**), and (**412, 612**).

To estimate the overall lane geometry information at the box **314** (i.e., the lane curvature κ, the vehicle's orientation with respect to the lane tangent θ, and the displacement to lane boundaries Δy), an estimate is needed for the position of center c.

Given a set of stripe segments $\{(e_k, t_k) | k=1, \ldots, K\}$. For each segment, (e_k, t_k) there is a normal (dashed lines in the diagram **400**) passing through c, i.e., $t_k^T(c - e_k) = 0$. Let $t_k = (t_{xk}, t_{yk})$. Therefore, finding c is equivalent to minimizing the following least squares:

$$\|Ec - \gamma\|, \quad E = \begin{bmatrix} t_{x1} & t_{y1} \\ t_{x2} & t_{x2} \\ \vdots & \vdots \\ t_{xK} & t_{yK} \end{bmatrix}, \quad \gamma = \begin{bmatrix} t_1^T e_1 \\ t_2^T e_2 \\ \vdots \\ t_K^T e_K \end{bmatrix} \tag{29}$$

The solution of the above least squares is $c = (E^TE)^{-1}E^T\gamma$. The curvature of the lane can be written as:

$$\kappa = \begin{cases} \dfrac{1}{\|c\|} & \text{if } c \text{ is on left side} \\ -\dfrac{1}{\|c\|} & \text{otherwise.} \end{cases} \tag{30}$$

The vehicle's orientation with respect to the lane tangent can be computed as:

$$\theta = a \tan 2(c_x, c_y) \tag{31}$$

where c_x is shown as dimension **426** and c_y is shown as dimension **428** in the diagram **400**.

FIG. **9** is a histogram **700** which shows an example of how the displacement to the lane boundaries can be computed. Let $\{z_j | j=1, \ldots, M\}$ denote the pixels of detected lane stripes. The histogram **700** is constructed which graphs the distance to the center c for all of these pixels (i.e., $d_j = \|z_j - c\|, j=1, \ldots, M$). The histogram **700** has an origin point **702**.

Displacement to left lane boundary y_L is distance **704** from the origin point **702** to the left local peak in the histogram **700**, while displacement to right lane boundary y_R is distance **706** from the origin point **702** to the right local peak.

Equations (29)-(31) estimate the lane using data from a single frame from the cameras **302** and **304**. The method can be extended to include tracking and data from vehicle dynamic sensors. Two such methods are proposed. For both methods, the state variables are defined as $s = (\kappa, \theta, \Delta y)$ where the variables are defined as the lane curvature (κ), vehicle orientation with respect to the tangent of the lane (θ), and displacements to the lane boundaries (Δy), respectively. Let the vehicle speed (v_H) and yaw rate (ω_H) denote measurements from the vehicle dynamic sensors.

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For the first method, a Kalman tracking procedure is used to estimate the lane parameters. FIG. **10** is a flow chart diagram **800** of the Kalman tracking method. The steps are as follows:

1) At box **802**, initialize the state vector s(0) with first measurement from the system **300** (Equations (29)-(31)), and choose a covariance matrix P(0) for s(0).

2) Wait at decision diamond **804** for new data to arrive; when the new measurement at time instant t arrives, at box **806** write the previous state vector as s(t−1); then at box **808** the predicted state s(t) at time instant t can be written as:

$$\kappa' = \kappa$$

$$\theta' = \theta - \omega_H \Delta T + \kappa v_H \Delta T$$

$$\Delta y' = \Delta y + v_H \Delta T \theta$$

where ΔT is the time increment, and the projected state vector s'(t)=[κ' θ' Δy'].

3) Also at the box **808**, the circle center is computed as:

$$c' = \left[\frac{1}{\kappa'} \sin\theta' \quad \frac{1}{\kappa'} \cos\theta' \right].$$

4) At box **810**, the detected stripes (e_k, t_k) from the cameras **302** and **304** are provided; then at box **812**, a gating operation is performed to identify outliers of the detected stripes, using the following criteria:

$$\frac{|(e_k - c')^T t_k|}{\|e_k - c'\|} < T$$

where T is a threshold value; a stripe will be treated as an outlier if the above is not true.

5) At box **814**, compute the current lane geometry information; for all stripes remaining after the gating of the box **812**, the least squares are minimized using Equation (29) to find the solution for the updated center ĉ; then κ_m and θ_m are computed through Equations (30)-(31), respectively, and displacements Δy_m through building the histogram.

6) At box **816**, perform a measurement correction; treat κ_m, θ_m, and Δy_m as the direct measurement of the state variables; the following measurement equations can be written:

$$\theta_m = \theta + w_{\theta_m}$$

$$\Delta y_m = \Delta y + w_{\Delta y_m}$$

$$\kappa_m = \kappa + w_{\kappa_m}$$

where $(w_{\theta_m} \ w_{\Delta y_m} \ w_{\kappa_m})^T$ is a zero-mean white Gaussian noise vector, whose covariance matrix is a function of the residue in the least squares minimization of Equation (29); then a Kalman filter is applied to the obtain the final output s(t) and the corresponding covariance matrix P(t).

7) At box **818**, output the updated lane geometry information, and go back to the decision diamond **804**.

The Kalman tracking procedure described above and on the flow chart diagram **800** represents the first method for computing lane curvature and vehicle orientation information, using images from the forward-view and rear-view cameras **302** and **304** and data from vehicle dynamics sensors. The second method uses a particle filter. FIG. **11** is a flow

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chart diagram **900** showing the particle filter method, which uses the following steps to compute the lane parameters:

1) At box **902**, initialize the state vector s(0) with a set of particles (random sample of geometry information): {(s$_i$(0), w$_i$)|i=1, . . . , M} and the weight

$$w_i = \frac{1}{M},$$

for i=1, . . . , M.

2) Wait at decision diamond **904** for new data to arrive; when the new measurement data at time instant t arrives, for each of the particles, κ_m, θ_m and Δy_m are calculated using the steps 2) to 5) of the Kalman tracker; that is;

   a. At box **906**, write the previous state vector as s(t−1).

   b. At box **908**, calculate the predicted state s(t); also compute the circle center c'.

   c. At box **910**, provide detected stripes from both cameras; at box **912**, perform a gating operation to identify outlier stripes.

   d. At box **914**, compute the current lane geometry information using Equations (29)-(31) and the histogram.

3) Then the value of the i-th particle becomes s'$_i$(t)=(κ$_m$, θ$_m$, Δy$_m$); let Δ_i denote the residue of the estimation for the i-th particle; at box **916**, compute the new weight of the particle as

$$w_i' = \exp\left(-\frac{\Delta_i^2}{2\sigma}\right),$$

where σ is a predefined constant.

4) At box **918**, compute the weighted average of the particle set ŝ(t) as:

$$\hat{s}(t) = \Sigma_{i=1}^M s_i(t) w_i / \Sigma_{i=1}^M w_i$$

and output ŝ(t).

5) At box **920**, apply importance re-sampling, a standard statistical procedure, to the updated particle set as {(s'$_i$(t), w'$_i$)|i=1, . . . , M}; this yields a set of random samples of the updated lane geometry information at box **922**.

6) Go to Step 2, the decision diamond **904**.

As described above and shown on the flow chart diagrams **800** and **900**, either the Kalman filter method or the particle filter method can be used to compute the lane geometry information—the lane curvature κ, the vehicle's orientation with respect to the lane tangent θ, and the displacement to lane boundaries Δy—using images from the forward-view and rear-view cameras **302** and **304**, and vehicle dynamics sensors, as input. The resultant lane geometry information can be used by downstream applications, such as a lane departure warning system.

The methods and systems disclosed herein, by using the image data available from a rear-view camera, and combining it with image data from a forward-view camera and other sensors, provide more robust capability for lane sensing or lateral control. The two-camera system not only makes use of more input data under normal conditions, but also provides a usable source of image data to allow operation of the system when conditions are unfavorable for forward-view imaging. Vehicle manufacturers and consumers can benefit from these systems, which take advantage of existing rear-view imaging capability in many vehicles to offer improved system performance and reliability, while incurring no new hardware-related costs.

The foregoing discussion discloses and describes merely exemplary embodiments of the present invention. One skilled in the art will readily recognize from such discussion and from the accompanying drawings and claims that various changes, modifications and variations can be made therein without departing from the spirit and scope of the invention as defined in the following claims.

What is claimed is:

1. A method for determining a vehicle's position in a lane, said method comprising:

providing data from a forward-view camera module onboard the vehicle;

providing data from a rear-view camera module onboard the vehicle;

providing data from vehicle dynamics sensors onboard the vehicle; and

fusing the data from the forward-view camera module, the rear-view camera module, and the vehicle dynamics sensors into a combined set of lane geometry information to determine the vehicle's position in the lane, including using a Kalman filter routine to jointly estimate the lane geometry information and misalignment angles of the forward-view camera module and the rear-view camera module, where the Kalman filter routine includes lane curvature, vehicle tangent angle to the lane, front bumper displacement to a lane boundary, and azimuth misalignment angles of the forward-view camera module and the rear-view camera module as state vector variables and simultaneously solves for all of the state vector variables.

2. The method of claim 1 wherein the lane geometry information includes lane curvature, vehicle orientation with respect to a tangent to the lane, and displacements to left and right lane boundaries.

3. The method of claim 1 wherein providing data from a forward-view camera module includes providing front lane geometry information from a front full-fledged lane sensing system, and providing data from a rear-view camera module includes providing rear lane geometry information from a rear full-fledged lane sensing system.

4. The method of claim 1 wherein providing data from a forward-view camera module includes providing forward image data from a front camera, and providing data from a rear-view camera module includes providing rear image data from a rear camera.

5. The method of claim 4 wherein fusing the data from the forward-view camera module, the rear-view camera module, and the vehicle dynamics sensors includes finding high intensity pixels in the forward image data and the rear image data, projecting the high intensity pixels onto a vehicle coordinate frame, detecting curbs and lane stripes from the high intensity pixels, linking the curbs and lane stripes into the lane, and tracking the lane geometry information.

6. The method of claim 4 wherein fusing the data from the forward-view camera module, the rear-view camera module, and the vehicle dynamics sensors includes using a Kalman filter.

7. The method of claim 4 wherein fusing the data from the forward-view camera module, the rear-view camera module, and the vehicle dynamics sensors includes using a particle filter.

8. The method of claim 5 wherein finding high intensity pixels in the forward image data and the rear image data includes using a Gaussian pyramid routine, where binary images at different spatial scales are subtracted from each other.

9. The method of claim 5 wherein projecting the high intensity pixels onto a vehicle coordinate frame includes using an iterative procedure to remove radial and tangential distortion, and a rotational and translational transformation procedure, to produce a plurality of high intensity pixels in the vehicle coordinate frame.

10. The method of claim 5 wherein detecting curbs and lane stripes from the high intensity pixels includes using a similarity graph and depth-first search routine, which clusters neighboring high intensity pixels into stripes.

11. The method of claim 10 wherein detecting curbs and lane stripes from the high intensity pixels also includes fitting the stripes with a line segment or an arc using a least-squares routine.

12. The method of claim 5 wherein linking the curbs and lane stripes into the lane includes finding a center of curvature of the lane using a least-squares routine applied to the curbs and lane stripes.

13. The method of claim 12 wherein tracking the lane geometry information includes computing displacements to left and right lane boundaries using a histogram routine, and computing lane curvature and vehicle orientation with respect to a tangent to the lane using the center of curvature.

14. A method for determining a vehicle's position in a lane, said method comprising:

providing image data from a forward-view camera onboard the vehicle;

providing image data from a rear-view camera onboard the vehicle; and

fusing the image data from the forward-view camera and the rear-view camera into a combined set of lane geometry information to determine the vehicle's position in the lane, including using a Kalman filter routine to jointly estimate the lane geometry information and misalignment angles of the forward-view camera and the rear-view camera, where the Kalman filter routine includes lane curvature, vehicle tangent angle to the lane, front bumper displacement to a lane boundary, and azimuth misalignment angles of the forward-view camera and the rear-view camera as state vector variables and simultaneously solves for all of the state vector variables.

15. The method of claim 14 wherein fusing the data from the forward-view camera and the rear-view camera includes finding high intensity pixels in the image data, projecting the high intensity pixels onto a vehicle coordinate frame, detecting curbs and lane stripes from the high intensity pixels, linking the curbs and lane stripes into the lane, and tracking the lane geometry information.

16. The method of claim 14 wherein the lane geometry information includes lane curvature, vehicle orientation with respect to a tangent to the lane, and displacements to left and right lane boundaries.

17. A system for determining a vehicle's position in a lane, said system comprising:

a first camera for capturing images of a forward view from the vehicle;

a second camera for capturing images of a rear view from the vehicle; and

a processor configured to receive the images from the first and second cameras and compute lane geometry information using a fusion of the images from the first and second cameras, including using a Kalman filter routine to jointly estimate the lane geometry information and misalignment angles of the first camera and the second camera, where the Kalman filter routine includes lane curvature, vehicle tangent angle to the lane, front

bumper displacement to a lane boundary, and azimuth misalignment angles of the first camera and the second camera as state vector variables and simultaneously solves for all of the state vector variables.

18. The system of claim **17** wherein the processor finds high intensity pixels in the images from the first and second cameras, projects the high intensity pixels onto a vehicle coordinate frame, detects curbs and lane stripes from the high intensity pixels, links the curbs and lane stripes into the lane, and tracks lane geometry information.

19. The method of claim **17** wherein the lane geometry information includes lane curvature, vehicle orientation with respect to a tangent to the lane, and displacements to left and right lane boundaries.

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